

# SANYO Semiconductors **DATA SHEET**



# Monolithic Digital IC For Fan Motor **3-phase Brushless Motor Driver**

#### **Overview**

The LB1991V is a 3-phase brushless motor driver IC that is optimal for driving the DC fan motor.

#### **Functions**

- 3-phase full-wave voltage drive technique (120° voltage-linear technique)
- Torque ripple correction circuit (overlap correction)
- Speed control technique based on motor voltage and current control
- Built-in FG comparators
- Built-in thermal shutdown circuit

### **Specifications**

#### Absolute Maximum Ratings at Ta = 25°C

Parameter	Symbol	Conditions	Ratings	Unit
Maximum supply voltage	V <sub>CC</sub> 1 max		10	V
	V <sub>CC</sub> 2 max		11	V
	V <sub>S</sub> max		11	V
Applied output voltage	V <sub>O</sub> max		V <sub>S</sub> +2	V
Maximum output current	I <sub>O</sub> max		1.0	А
Allowable power dissipation	Pd max	Independent IC	440	mW
Operating temperature	Topr		-20 to +75	°C
Storage temperature	Tstg		-55 to +150	°C

#### Allowable Operating Ranges at Ta = 25°C

Parameter	Symbol	Conditions	Ratings	Unit
Supply voltage	V <sub>CC</sub> 1	$V_{CC}1 \le V_{CC}2$	2.7 to 6.0	V
	V <sub>CC</sub> 2		3.5 to 9.0	V
	٧ <sub>S</sub>		Up to V <sub>CC</sub> 2	V
Hall input amplitude	V <sub>HALL</sub>	Between Hall effect element inputs	±20 to ±80	mVp-p

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# LB1991V

# **Electrical Characteristics** at Ta = 25°C, $V_{CC}1 = 3V$ , $V_{CC}2 = 4.75V$ , $V_S = 1.5V$

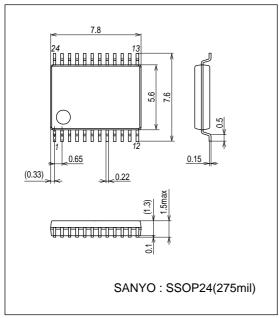
Parameter	Symbol Conditions	Ratings			Unit	
	Cymbol		min	typ	max	Unit
Supply Current		1				
V <sub>CC</sub> 1 current drain	I <sub>CC</sub> 1	I <sub>OUT</sub> = 100mA		3	5	mA
V <sub>CC</sub> 2 current drain	I <sub>CC</sub> 2	I <sub>OUT</sub> = 100mA		7.0	10.0	mA
V <sub>CC</sub> 1 quiescent current	I <sub>CC</sub> 1Q	V <sub>STBY</sub> = 0V		1.5	3.0	mA
V <sub>CC</sub> 2 quiescent current	I <sub>CC</sub> 2Q	V <sub>STBY</sub> = 0V			100	μA
VS quiescent current	I <sub>S</sub> Q	V <sub>STBY</sub> = 0V		75	100	μA
VX1		-				
High side residual voltage	V <sub>XH</sub> 1	I <sub>OUT</sub> = 0.2A	0.15	0.22	0.29	V
Low side residual voltage	V <sub>XL</sub> 1	I <sub>OUT</sub> = 0.2A	0.15	0.20	0.25	V
VX2						
High side residual voltage	V <sub>XH</sub> 2	I <sub>OUT</sub> = 0.5A		0.25	0.40	V
Low side residual voltage	V <sub>XL</sub> 2	I <sub>OUT</sub> = 0.5A		0.25	0.40	V
Output saturation voltage	V <sub>O</sub> (sat)	I <sub>OUT</sub> = 0.8A, Sink + Source			1.4	V
Overlap	O.L	$R_L = 39\Omega \times 3$ , Rangle = 20k $\Omega$ *2	72	80	87	%
High/low overlap difference	∆0.L	(Average upper side overlap) – (Average lower side overlap) *2	-8		+8	%
Hall Amplifiers			Ł			
Input offset voltage	VHOFF	Design target *1	-5		+5	m\
Common-mode input voltage range	VHCM	Rangle = $20k\Omega$	0.95		2.1	V
I/O voltage gain	V <sub>GVH</sub>	Rangle = $20k\Omega$	25.5	28.5	31.5	dB
Standby Pin						
High-level voltage	VSTH		2.5			V
Low-level voltage	VSTL				0.4	V
Input current	ISTIN	V <sub>STBY</sub> = 3V		25	40	μA
Leakage current	ISTLK	V <sub>STBY</sub> = 0V			-30	μA
FRC Pin	0.12.0					
High-level voltage	VFRCH		2.5			V
Low-level voltage	VFRCL				0.4	V
Input current	IFRCIN	V <sub>FRC</sub> = 3V		25	30	μA
Leakage current	IFRCLK	V <sub>FRC</sub> = 0V			-30	μA
VH	TROLK					
Hall supply voltage	V <sub>HALL</sub>	I <sub>H</sub> = 5mA, VH(+) – VH(–)	0.85	0.95	1.05	V
(-) pin voltage	V <sub>H</sub> (–)	$I_{\rm H} = 5 {\rm mA}$	0.81	0.88	0.95	V
FG Comparator		11 -				
Input offset voltage	VFGOFF		-3		+3	m∖
Input bias voltage	I <sub>bFG</sub>	$V_{FGIN}^+ = V_{FGIN}^- = 1.5V$			500	nA
Input bias current offset		$V_{FGIN}^+ = V_{FGIN}^- = 1.5V$	-100		+100	nA
Common-mode input voltage range			1.2		2.5	V
Output high-level voltage	VFGCM	At the internal pull-up resistors	2.8		2.0	v V
	VFGOH		2.0		0.2	V
Output low-level voltage	VFGOL	At the internal pull-up resistors		400	0.2	
Voltage gain	VGFG	Design target *1		100	-	dB
Output current (sink)	IFGOS	For the output pin low level			5	mA
Thermal shutdown	TOD				I	
Operating temperature	TSD	Design target *1		180		°C
Temperature hysteresis	∆TSD	Design target *1		20		°C

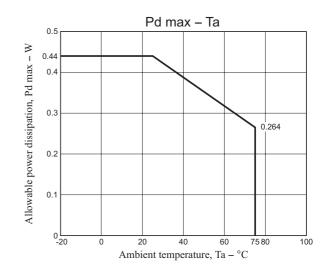
\*1: Design target values in the conditions column are not tested.

 $^{\ast}$  2: The standard for overlap is the value as measured.

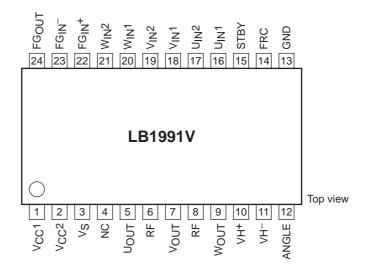
## Package Dimensions

unit : mm (typ) 3175C





# **Pin Assignment**

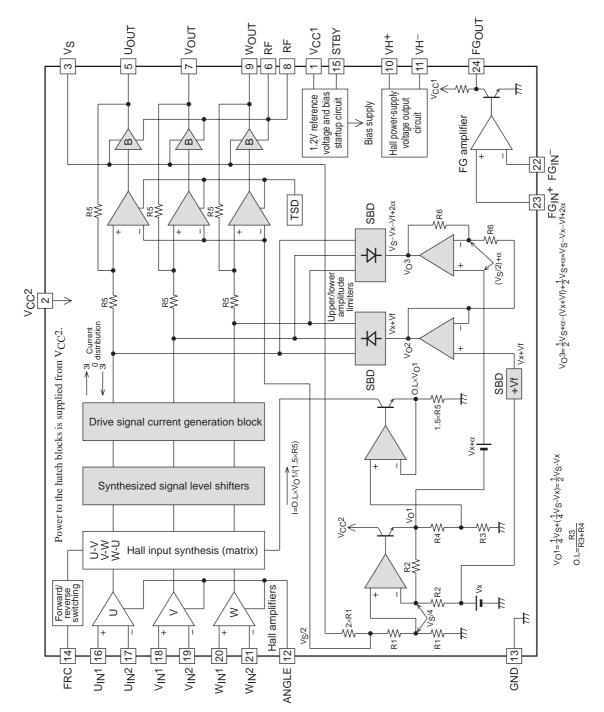


# **Truth Table**

	Source phase $\rightarrow$ Sink phase	Hall input			FRC
			V	W	FRC
1	$V\toW$	н		L	Н
I	$W\toV$	Г	Н	L	L
2	$U\toW$	н	L	L	Н
2	$W\toU$	п	L	L	L
3	$U\toV$	Н	L	н	Н
3	$V\toU$				L
4	$W\toV$	L	L	н	Н
4	$V \to W$	L	L	Г	L
-	$W\toU$	L			Н
5	$U\toW$	L	Н	Н	L
6	$V\toU$	L	н	L	Н
6	$U\toV$	L	п	L	L

Note: The "H" entries in the FRC column indicate a voltage of 2.50V or higher, and the "L" entries indicate a voltage of 0.4V or lower. (When V<sub>CC</sub>1 is 3V.) At the Hall inputs, for each phase a high-level input is the state where the (+) input is 0.02V or higher than the (-) input. Similarly, a low-level input is the state where the (+) input is 0.02V or lower than the (-) input.

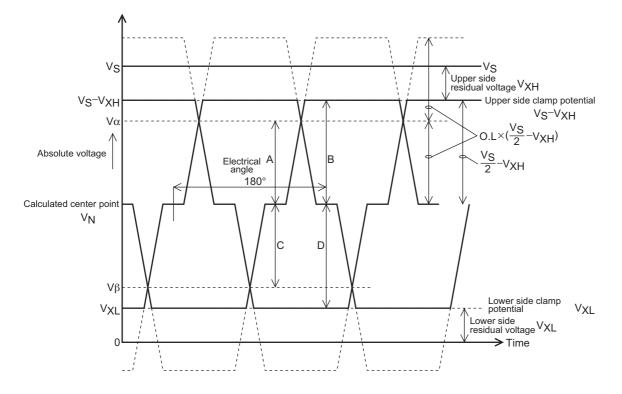
## **Block Diagram**



# **Pin Function**

Pin No.	Pin name	Pin function	Equivalent circuit
1	V <sub>CC</sub> 1	Supply voltage for all circuits other than the IC internal output block and the amplitude control block.	
2	V <sub>CC</sub> 2	Supply voltage for the IC internal output control block and the amplitude control block.	
3	۷ <sub>S</sub>	Motor drive power supply. The voltage applied to this pin must not exceed $V_{\mbox{CC}}2.$	2 V <sub>CC</sub> 2 ≥10kΩ - 3 V <sub>S</sub>
5	UOUT	U phase output.	
7	VOUT	V phase output.	$1/4 \times V_S$ 5 Each OUT
9	WOUT	W phase output. (These outputs include built-in spark killer diodes.)	$\frac{\underset{5}{\overset{5}{}}_{5k\Omega}}{{}_{77}} \qquad \qquad$
6,8	RF	Ground for the output power transistors.	(8)
10	VH+	Hall element bias voltage supply. A voltage that is typically 0.95V is generated between the VH <sup>+</sup> and VH <sup>-</sup> pins (When I <sub>H</sub> is 5mA).	
11	VH−		
13	GND	Ground for circuits other than the output transistor. The RF pin potential is the lowest output transistor potential.	
14	FRC	Forward/reverse selection. Applications can select motor forward or reverse direction rotation using this pin. (This pin has hysteresis characteristics.)	
15	STBY	Selects the bias supply for all circuits other than the FG comparators. The bias supply is cut when this pin is set to the low level.	
16 17	U <sub>IN</sub> 1 U <sub>IN</sub> 2	U phase Hall element input. The logic high level is the state where the IN <sup>+</sup> voltage is greater than the IN <sup>-</sup> voltage.	
18 19	V <sub>IN</sub> 1 V <sub>IN</sub> 2	V phase Hall element input. The logic high level is the state where the $IN^+$ voltage is greater than the $IN^-$ voltage.	$4k\Omega \lesssim 4k\Omega \lesssim 200\Omega (18,20)$
20 21	W <sub>IN</sub> 1 W <sub>IN</sub> 2	W phase Hall element input. The logic high level is the state where the IN <sup>+</sup> voltage is greater than the IN <sup>-</sup> voltage.	1.2V typ $\downarrow$
12	ANGLE	Hall input/output gain control. The gain is controlled by the resistor connected between this pin and ground.	
22	FG <sub>IN</sub> +	FG comparator non-inverting inputs. There is no internally applied bias.	
23	FG <sub>IN</sub> <sup>-</sup>	FG comparator inverting inputs. There is no internally applied bias.	$\begin{bmatrix} G_{IN}^{-} & & & & & & & & & & & & & & & & & & &$
24	FG <sub>OUT</sub>	FG comparator outputs. There is an internal $20k\Omega$ resistor load.	

### **Overlap Generation and Calculation Method**



#### **Overlap Generation**

Since the voltage generated in the amplitude control block is, taking the center point as the reference,  $2 \times \langle \text{overlap} \rangle \times (1/2 \text{ V}_S - \text{V}_X)$  on one side, the intersection point of the waveform will be  $\langle \text{overlap} \rangle \times (1/2 \text{ V}_S - \text{V}_X)$  from the center point.

To clamp that waveform at (1/2 V<sub>S</sub> – V<sub>X</sub>) referenced to the center point the overlap must be:  $A/B \times 100 = \langle overlap \rangle \times 100$  (%).

#### **Overlap Calculation**

• Upper side overlap Calculated center point:  $V_N = \frac{(V_S - V_{XH} - V_{XL})}{2} + V_{XL} = \frac{(V_S - V_{XH} + V_{XL})}{2}$ Since  $A = V\alpha - V_N$ ,  $B = V_S - V_{XH} - V_N$ , the upper side overlap will be:  $\langle \text{overlap} \rangle = \frac{A}{B} = \frac{V\alpha - ((V_S - V_{XH} + V_{XL})/2)}{V_S - V_{XH} - ((V_S - V_{XH} + V_{XL})/2)} \times 100$ 

Which can be calculated as:

$$=\frac{2V\alpha - (V_{S} - V_{XH}) - V_{XL}}{(V_{S} - V_{XH}) - V_{XL}} \times 100(\%)$$

• Lower side overlap

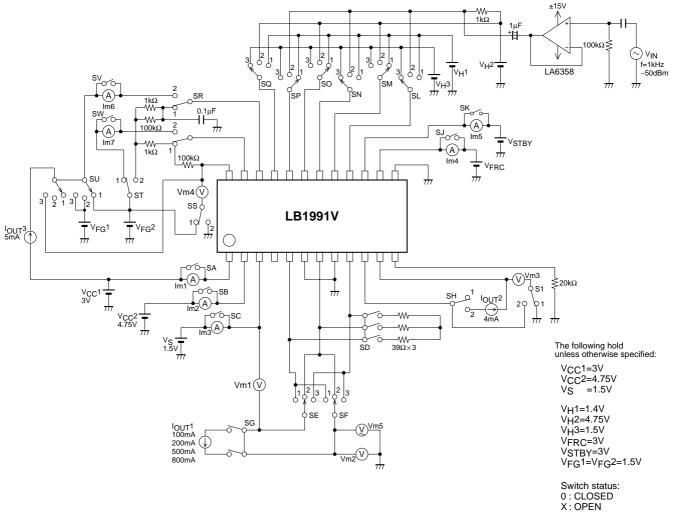
Since  $C = V_N - V\beta$ , and  $D = V_N - V_{XL}$ , the lower side overlap will be:

$$< \text{overlap} > = \frac{C}{D} = \frac{((V_{S} - V_{XH} + V_{XL})/2) - V\beta}{((V_{S} - V_{XH} + V_{XL})/2) - V_{XL}} \times 100$$

Which can be calculated as:

$$=\frac{(V_{S}-V_{XH})+V_{XL}-2V\beta}{(V_{S}-V_{XH})-V_{XL}}\times100(\%)$$

## **Test Circuit**



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